

# Launch loads in space applications – Analysis and recommendations for design optimization

” **The systematic analysis of the effects of launch loads is a key part of the process to select the best bearing solution for a given application.** „

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Space consists of everything from the big bang and the creation of the Universe to the galaxies and planets, right down to objects around 10 cm<sup>3</sup> we call satellites. Satellites are designed to fulfil specific tasks like Earth observation, communication, navigation and of course human life support. They are deployed normally in a low Earth orbit to allow real time data transfer. According to the Bryce Tech reports around 40% of small satellites were launched in 2020 alone and the prediction is that around 1400 small satellites per year will be launched over the next ten years. Therefore, it is clear the business potential is significant.

This increasing number of satellites means an equally large increase in the number of subsystems on board. For example LIDAR sensors for pose estimation, reaction wheels and gyros for positioning and actuation mechanisms for solar panels. In each of these applications, to achieve the desired accuracy of operation, super precision ball bearings from GRW are employed. These bearings need to be carefully designed to avoid common failure mechanisms. One important but often overlooked area is the ability of the bearing to withstand the significant shock loading during launch and sometimes re-entry. If the bearing design somehow overlooks or underestimates these loads during the system design, this can result in catastrophic results. Such a bearing failure can cause whole system failure.

This article outlines some of the lessons learnt both positive and negative by GRW over years of design experience in space applications. A standardized strategy to

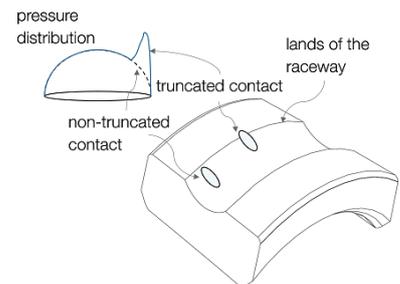
understand what happens when shock loads occur and their systematic investigation is introduced here. In conclusion, the article provides general guidelines and recommendations that can help the space community to avoid early design errors, to optimize their solution and assist in selection of the correct bearing for the application.

## Understanding the Issues

Clarification of the following issues helps to define the objectives:

- Can the momentarily occurring shock loads seen during launch be accommodated in such a way that they will not affect the normal operation of the bearing during its normal duty cycle?
- Is the level of damage, under these shock loads, that might occur to the bearing raceway and lands due to the ball moving to the track edge, so called truncation, be considered acceptable (refer to Figure 1)?
- Do we need to employ a bigger size of bearing for the application?

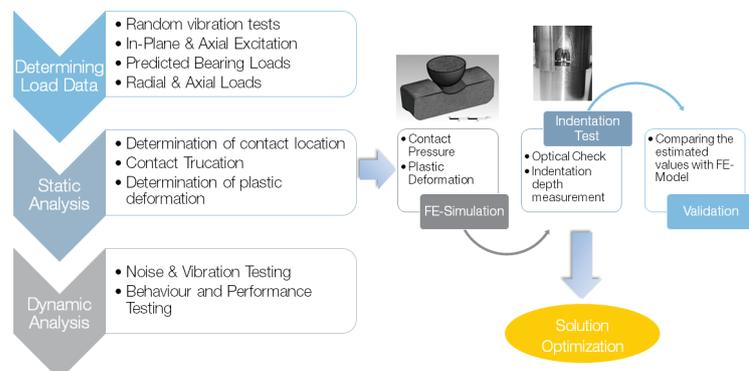
Therefore, I tried to provide the convincing explanation to the issues mentioned.



— Figure 1: Raceways showing the truncated and non-truncated contact along with the pressure distribution profile [FL01]

## Methods and Techniques for Bearing Design and Selection

GRW possesses the expertise and employs various simulation and experimental techniques to investigate the bearing quasi-statically as well as dynamically. This helps the designer to critically consider the operating scenario in their design process and accordingly select the bearings that suit the application. So, how do we do it? The strategy is standardized and can be easily self-explained through the following process chart (refer to Figure 2).



— Figure 2: A process chart for a systematic analysis of effects of shock loads on the bearing performance and bearing selection

Mesys bearing calculation program helps to determine the overall load distribution inside the bearing (Figure 3 a) & b)) and based on that performs the bearing life calculation as per ISO 281. Together with this, program also estimates the influences of bearing and shaft-housing tolerances and temperatures on the resulting operating clearance in the mounting situation.

Similarly, Figure 4 shows the FE-Ansys full bearing model, which is then reduced to a single ball-raceway contact (Figure 4. b) to have an advantage of computation and convergence efficiency. This replicates the exact loading scenario and aims to simulate the detailed contact situations to determine the contact stiffness and deformation (Figure 4. c).

Based on the loading situation, resulting contact angles and pressure distribution (refer to Figure 3 b) can be determined. This makes possible to identify whether, under the shock loads, truncation of the contact ellipse occurred or not. Because this is a critical situation, that one should avoid. The maximum resulting rolling element load is extracted and used as an input for FE-Contact simulation.

In this way, we can make a qualitative as well as a quantitative statement whether the given shock loads tend to cause the plastic deformation or not.

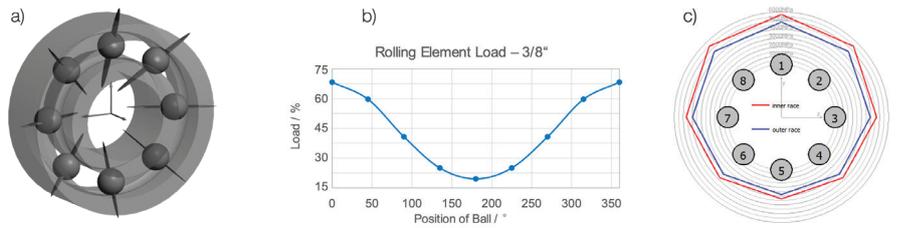
Nevertheless, an indentation test setup (see Figure 5) is developed to verify the simulation model. A single ball is pressed against a ring to find the impression. The indentation is optically investigated, measured, and evaluated (see Figure 5 d).

Static testing is followed by the dynamic noise and vibration testing to investigate the behavior and performance. It is made assured if in case under the shock loads truncation occurred, it is away from the running track and the operating behavior of the bearing will not be influenced when the bearing is operated under the normal operating conditions.

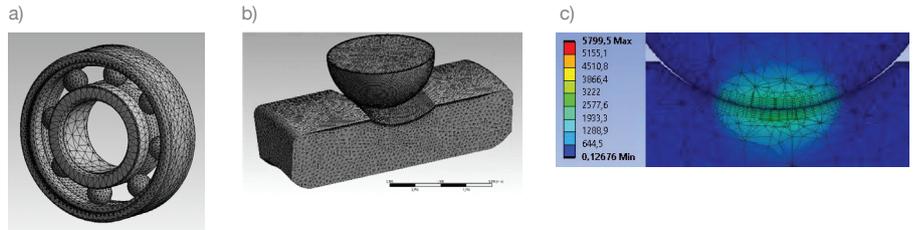
**Recommendations**

By performing the critical analysis, we can make recommendations; say for example, for the right bearing selection in the following ways:

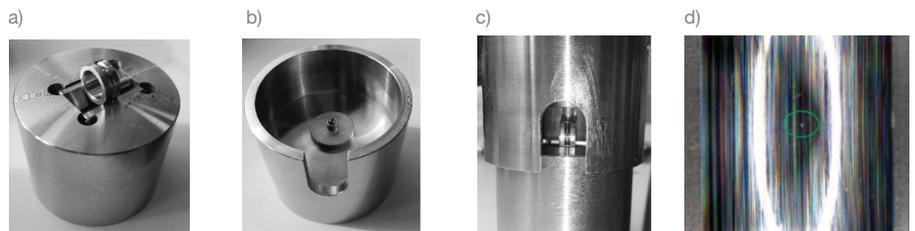
- Design Changes: We need to think of adapting the shoulder height of the



— Figure 3: Mesys Bearing – Calculation; a) Mesys-Bearing Model - Loading situation inside the bearing; b) Contact loads at each ball-raceway contact; c) Pressure distribution under the combined load for deep groove ball bearing of type 3/8", radial load 1200 N, axial load 1500 N



— Figure 4: FE-Ansys Simulation; a) FE-Full bearing model 3/8" deep groove ball bearing; b) Reduced model of ball-raceway contact with a fine mesh at surface & subsurface contact; c) Exemplary contact pressure for the maximum load of 800 N



— Figure 5: Indentation test set-up; a) Prism holding the ring; b) Punch holding the ball; c) Assembled situation; d) Indentation on the ring

- raceway lands to avoid the truncation of the contact region if we recognize the problem with the selected bearing.
- Material Selection: In case the selected bearing is not able to ensure the expected static load capacity, then one must think of considering other advanced bearing materials that offer a higher static load rating.
- Bearing Dimensions: Even after taking into consideration the design and material changes, still, we are unable to achieve the static load rating that can withstand the expected shock loads, then we can think of the next bigger size of the bearing in the series and run the whole analysis systematically as mentioned to make sure that the customer requirements fulfill. Nevertheless, you have to make sure that bigger size bearings cannot always be the right solution, as you have to take into account the size-to-weight ratio of the applications.

These guidelines and recommendations from GRW can certainly help the designer to consider the factors arising due to shock loads, accordingly find the suitable solution of bearing selection for their applications, and avoid the potential failures of the systems.

More information can be found at [www.grw.de](http://www.grw.de)



<sup>1</sup> Frantz, P.P.; Leveille, A.R.: "An Approach to Predicting the Threshold of Damage to an Angular Contact Bearing During Truncation", Space and Missile Systems Center Air Force Materiel Command, 2430 E. El Segundo Boulevard, Los Angeles Air Force Base, CA 90245, 2001.